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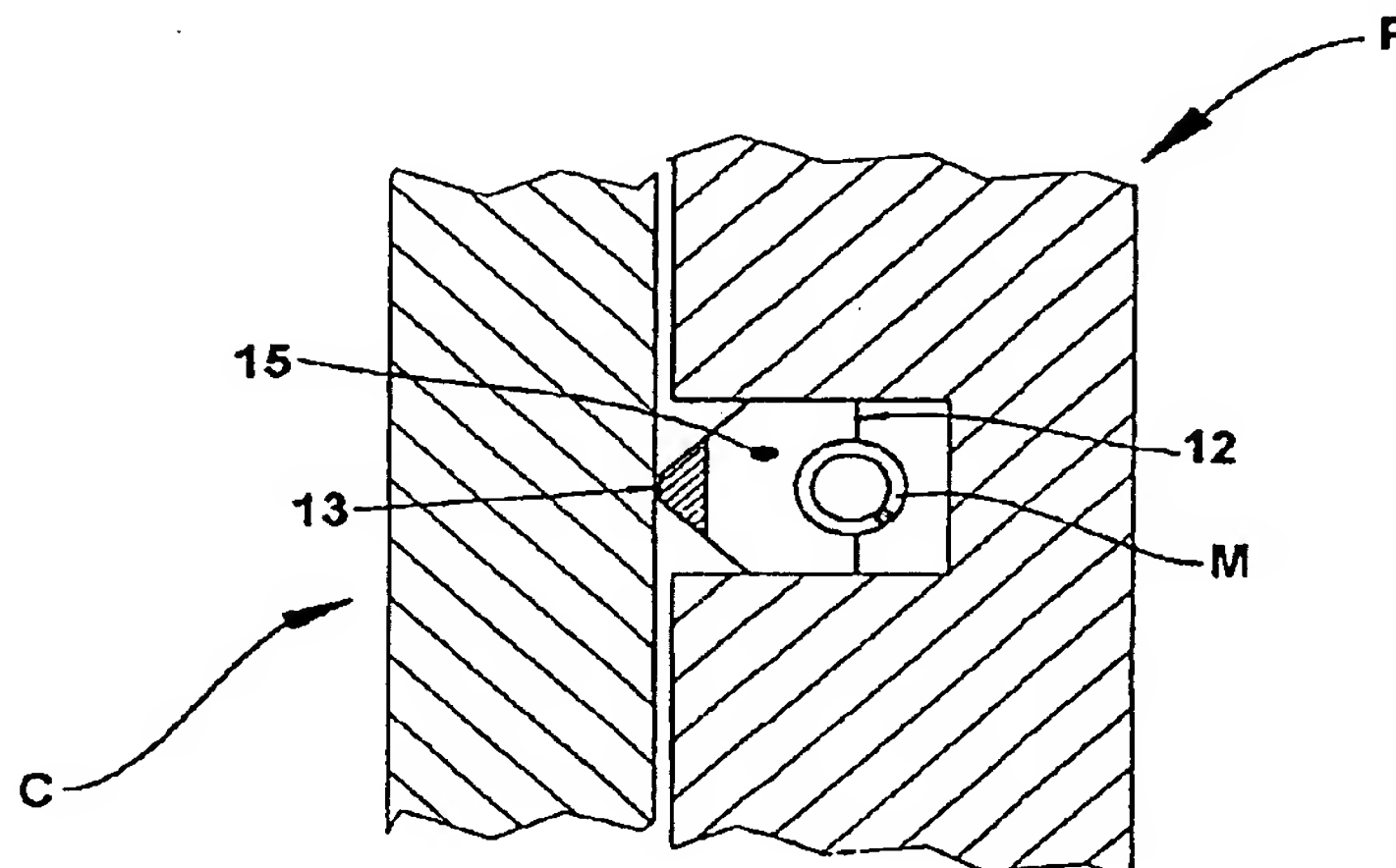
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[Continued on next page]

(54) Title: **OIL RING FOR AN INTERNAL COMBUSTION ENGINE**



(57) Abstract: An oil ring for an internal combustion engine, comprising a metallic annular body (10) to be mounted around a piston (P) reciprocating inside a cylinder (C) of the engine, said annular body (10) having opposite lateral faces (11), an internal face (12) onto which will be seated a resilient expander (M), and an external contact face (13) to be seated against the internal face of the cylinder (C) and having a height (h) that is substantially smaller than the height (H) of the internal face (12). Each lateral face (11) is defined by one or more lateral face portions (11a, 11b), which are designed to reduce the moment of inertia of the annular body (10), giving higher conformability to the latter. Preferentially, but not exclusively, the annular body (10) can be further provided with channels (15, 16), extended along at least part of the ring height and which are radially spaced back in relation to the external contact face (13).

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OIL RING FOR AN INTERNAL COMBUSTION ENGINE

Field of the Invention

The present invention refers to an oil flow control ring for the piston of internal combustion engines, said ring having optimized specific pressure and high conformability.

Background of the Invention

Until the 1920's, practically all the internal combustion engines used only compression rings. Engine rotations were low and the compression rings were sufficient to control the small amounts of oil sent by the connecting rods to the cylinder walls.

With the use of higher rotation rate engines and the introduction of the pressurized lubrication system, the use of a specific ring was required to control the large amounts of oil sent against the cylinder walls. At that time, a ring named oil flow controller was developed. Such ring is characterized by having, on the external face thereof, two contact surfaces with the cylinder wall, which are separated by a channel containing radial slots for oil flow drainage. To increase the tangential load and ring conformability, a spring housing has been added to the internal face. From that time on, there has not been a great evolution in the basic shape, except for the rings with the external contact face presenting a conical profile for better control of the lubricant oil consumption during the break-in period of the engine.

The oil flow control ring must present two main functional characteristics: scraping the oil from the cylinder wall towards the crankcase of the engine, and maintaining a sufficient amount of oil to the compression rings above them, so that the oil film is maintained between the rings and the cylinders all the time.

The efficiency with which an oil flow control ring performs such functions results from the following factors: capacity of rapidly seating on the cylinder; the geometry of the contact face; the pressure against the cylinder walls; the dynamics of oil removal and drainage; and the ability to rapidly conform to the variations of the cylinder profile.

Nevertheless, the known prior art technology has limitations as to the optimization of friction losses and oil consumption.

It has been found that nearly 25% of friction losses of an engine are due to the rings, and 70% of said losses come from the oil ring under operation, mainly due to its high tangential load. Thus, any study relating the friction reduction in a set of piston rings should be started by the oil flow control ring. The tangential load is directly related to the formula of the specific pressure that the ring contact face exerts against the cylinder wall. This pressure is one of the main parameters of oil flow control and is expressed by:

$$P_0 = \frac{2.Ft}{d1.c} \quad (1)$$

P_0 = specific pressure

Ft = tangential load

$d1$ = nominal diameter of the ring

c = dimension of the ring contact face with the cylinder

Experiments and literature show that the lower the specific pressure the higher will be the oil consumption. Thus, in order to maintain the same oil control conditions and reduce the friction loss by reducing the tangential load, a dimension reduction in the ring contact face with the cylinder is required to maintain the same specific pressure.

For example, considering an oil flow control ring with a coil spring (in a Diesel engine) and with a 102.0 mm nominal diameter, there is the following variation of the specific pressure as a function of the usual manufacturing tolerances:

$$d_1 = 102.0 \text{ mm}$$

$$F_t = 54 + 40\% N$$

$$h = c/2 = 0.40 \pm 0.10 \text{ mm}$$

$$F_t \text{ min.} = 54 \text{ N} \quad F_t \text{ max.} = 76 \text{ mm}$$

$$h \text{ min.} = 0.30 \text{ mm} \quad h \text{ max.} = 0.50 \text{ mm}$$

From formula (1) above there would be:

$$P_0 \text{ min.} = 1.06 \text{ N/mm}^2$$

$$P_0 \text{ max.} = 2.48 \text{ N/mm}^2$$

which would give a variation of about 134% from the minimum value. As a function of this considerable difference in the specific pressure, a series of tests in dynamometer were performed, using oil flow control rings under the minimum specific pressure conditions, as compared to rings with maximum specific pressure, in order to study the performance of the engine in these two extremes (see table 1).

TABLE 1

Diesel engine - 4 cyl., 60kW - 3000 r.p.m		
	$P_0 = 1.06 \text{ N/mm}^2$	$P_0 = 2.48 \text{ N/mm}^2$
Lubricant oil consumption	0.57	0.26
Friction loss Wilan's lines (kW)	19.8	21.1

These results showed a large variation on engine's performance, mainly relating to oil consumption, partially caused by the dimensional tolerance of the contact surface. It should be noted that, by increasing the specific pressure, the consumption was reduced to half, but generating the undesired higher friction effect.

In addition to specific pressure, ring conformability is one of the most significant characteristics for oil flow control.

Ring conformability is a parameter that indicates the better or worse capacity of the ring to adapt to the possible deformations or diametral variations of the cylinder, thus maintaining its scraping and sealing capacity. The ring conformability is represented by the conformability factor that is expressed by the following mathematical relation:

$$k = \frac{F_t \cdot (d_1 - r_1)^2}{4 \cdot E \cdot I}$$

k = conformability factor

F_t = tangential load

d₁ = nominal diameter of the ring

r₁ = ring radial wall thickness

E = modulus of elasticity

I = moment of inertia

The example below illustrates the conformability calculation presented herein:

By using mean dimensional values of an Otto cycle ring with a 67.1 mm diameter:

F_t = 36.0 N

d₁ = 67.1 mm

r₁ = 2.23 mm

E = 160 GPa

I = 0.34

The higher the k factor, the higher will be the capacity of the ring to adapt to cylinder deformations and better will be the oil flow control. Since it is not desirable to increase the tangential load due to the increase of friction losses, only the modulus of elasticity and the geometrical shape of the ring remain available to improve the conformability.

Objects of the Invention

The general object of the present invention is to provide an oil ring for internal combustion engines having high conformability and optimized specific pressure to provide high oil scraping efficiency without increasing the friction losses.

A further object of the invention is to provide an oil ring such as cited above that presents adequate drainage dynamics of the scraped oil.

Still a further object of the present invention is to provide an oil ring such as cited above that can be made with minimum manufacturing operations.

Summary of the Invention

As mentioned above, the invention refers to an oil ring for internal combustion engines comprising an annular body to be mounted around a piston that reciprocates inside a cylinder of the engine.

As known, the annular body has opposite lateral faces, an internal face, defining a support onto which will be seated a resilient expander generally in the form of a metallic spring, and an external contact face to be seated against the internal face of the cylinder.

According to the invention, the external contact face is defined by a single continuous surface extension of the annular body presenting, in the axial direction, a height that is substantially smaller than the height of the internal face, each lateral face being defined by at least one lateral face portion that is designed to reduce the moment of inertia of the annular body towards its axis and its center of mass.

The construction proposed by the invention not only allows for the reduction of the total height of the ring, as it uses only one external contact face, but also the reduction of friction, by reducing the tangential load, without causing damages to the specific pressure that is required for a desired

scraping efficiency, since the contact face is conveniently correspondingly reduced.

Brief description of the drawings

The invention will be described below, with reference
5 to the appended drawings, in which:

Figure 1 is a partial plan view of the oil ring of the present invention, according to a first embodiment;

Figure 2 is an enlarged cross-sectional view of the ring, taken according to line II-II of figure 1;

10 Figure 3 is a similar view to that of figure 2, but taken according to line III-III of figure 1 and illustrating the annular body housed in a piston inside a cylinder and receiving a resilient expander in its internal face;

15 Figures 4, 5 and 6 are similar views to that of figure 2, but illustrating three possible alternatives for the profile of the external contact face of the annular body;

Figure 7 is a plan view of the oil ring of the present
20 invention, similar to that of figure 1, but illustrating another embodiment for the ring; and

Figure 8 is an enlarged cross-sectional view of the other embodiment of the ring, taken according to line VIII-VIII of figure 7.

25 Detailed Description of the Illustrated Embodiments

As illustrated, the oil ring object of the present invention is made of steel, cast iron, another metal alloy, polymeric material or any other suitable material, comprising an annular body 10 to be mounted
30 to a respective groove of a piston P designed to reciprocate inside a cylinder C of the internal combustion engine.

The annular body 10 has a pair of end faces 11, which are opposite and generally parallel to each other and
35 orthogonal to the axial axis of the ring, an internal

face 12, and an external contact face 13 to be seated against the internal face of the cylinder C, in order to scrape the lubricant oil that is conducted to this region upon operation of the engine. The internal face
5 12 of the annular body 10 defines a support, generally in the form of a groove 12a, for example having a "V" or "U" profile or combinations of these shapes, onto which will be seated a resilient expander "M" generally defined by a metallic spring that is
10 dimensioned to exert a determined expanding radial force against the annular body 10.

According to the invention, the external contact face 13 is defined by a single continuous surface extension of the annular body 10 presenting, in the axial
15 direction, a height h that is substantially smaller than the height H of the internal face 12. Preferably, the height h of the external contact face 13 is at maximum about half the height H of the internal face 12, so as to allow a corresponding reduction of the
20 tangential load F_t that is necessary to maintain the desired specific pressure " P_0 " of the external contact face 13 against the cylinder C.

The construction proposed herein allows the manufacture of a narrower external contact face with
25 reduced dimensional tolerance in relation to the prior art, minimizing the variation of the specific pressure P_0 and improving the oil flow control. By maintaining only one contact surface on the external contact face 13 the specific pressure variations occurring nowadays
30 in the oil rings with two contact surfaces is reduced to half. From the data of the example given above, the embodiment proposed herein has the following specific pressure variation:

$$d1 = 102.0 \text{ mm}$$

35 $F_t = 54 + 40\% \text{ (N)}$

$h = c = 0.8 \pm 0.10$ (mm)

Ft min. = 54 N Ft max. = 76 N

h min. = 0.7 mm h max. = 0.9 mm

From formula (1) above there would be:

5 P_0 min. = 1.18 N/mm²

P_0 max. = 2.13 N/mm²

As it can be observed from the example above, the new constructive solution conducts to a specific pressure variation of about 80% versus 134% of the presently
10 known construction.

In addition to the dimensional aspect mentioned above, the annular body 10 has its lateral faces 11 (or at least one of them) configured to reduce the moment of inertia of the annular body 10 towards its axial axis
15 and its center of mass, imparting higher conformability to the ring.

In the illustrated embodiments, each lateral face 11 of the annular body 10 is defined by a first lateral face portion 11a, which is orthogonal to the axial
20 axis of the annular body 10 and maintains the height of the latter equal to the height H of the internal face 12, and the first lateral face portions 11a of both lateral faces 11 are consequently parallel to each other. Each lateral face 11 further comprises a
25 second lateral face portion 11b, radially outwardly extending from the first lateral face portion 11a towards the adjacent edge of the external contact face 13 of the annular body 10. Still according to the illustrated embodiments, both second lateral face
30 portions 11b are mutually convergent towards the external contact face 13.

While the drawings illustrate only one constructive form of the lateral faces 11, it should be understood that they may present other configurations. For
35 example, only one of the lateral faces 11 can be

defined by two distinct lateral face portions. One of said lateral faces 11 would be integrally defined by a first lateral face portion 11a, while the other lateral face 11 would be partially defined by a first lateral face portion 11a and completed by a second lateral face portion 11b designed to reduce the height of the annular body 10 towards the external contact face 13. In a possible alternative construction, said other lateral face 11 would be integrally defined by a second lateral face portion 11b extending from the internal face 12 up to the external contact face 13 and producing the necessary reduction in the height of the annular body 10.

It should be further understood that other geometrical shapes could be used, provided that they result in the same effect in terms of conformability factor.

For example, we can compare the same Otto oil ring with a diameter of 67.1 mm used in the previous conformability calculation:

$F_t = 36.0 \text{ N}$

$d_1 = 67.1 \text{ mm}$

$r_1 = 2.23 \text{ mm}$

$E = 160 \text{ GPa}$

$I = 0.241 \text{ mm}^4$

$K = 0.98$ (188% better)

Thus, in relation to the present technique, the ring geometry improves the capacity of the ring to adapt to cylinder deformations, consequently improving oil flow control.

The construction of the present invention makes possible to induce torsion of the ring when confined. Such action can be useful as an aid to control consumption of lubricant oil and cannot be applied to normal oil rings, since their contact faces have two contact surfaces and the torsion would impair the

contact of one of said faces, consequently impairing the performance of the ring functions. Also, by having the contact surface as the only constructive element of its external contact face, as opposed to the prior art that requires the presence of two contact surfaces and a recess, the innovation easily permits to obtain rings with a smaller height than that of the prior art. Thus, there is provided an increase in ring conformability, concomitantly with weight reduction of the pistons and the resulting benefits.

In the embodiment illustrated in figures 1, 2 and 3, the external contact face 13 is cylindrical and generally orthogonal and symmetrical in relation to a plane orthogonal to the axial axis of the annular body 10 and medianly intercepting the latter.

However, the external contact face 13 may be conical, such as illustrated in figure 4, and it may further contain, close to its peripheral edge of larger diameter, a lowered step 13a, as illustrated in figure 5. Another exemplary embodiment for the external contact face 13 is illustrated in figure 6, where said external contact face 13 is defined by a surface having a convex arcuated profile, which can be also symmetrical in relation to said median plane orthogonal to the axial axis of the annular body 10.

The annular body 10 can be further provided with channels 15, 16, extended along at least part of the ring hight and which are radially spaced back in relation to the external contact face 13. In the constructions illustrated in figures 1, 2, 3 and 4, the channels 15 provide fluid communication between lateral face portions 11b, which are opposite to each other and spaced from the adjacent walls of the piston P, upon mounting the annular body 10 thereto. This construction of the channels 15 allows the oil to be

scraped from the wall of the cylinder C and drained to the crankcase in a freer path. However, it should be understood that channels 15, 16 do not need to provide fluid communication between said opposite lateral face portions 11b of the ring, spaced from the adjacent walls of de piston P, as shown in figures 5, 6, 7 and 8.

Being the annular body 10 provided with the groove 12a in its internal face 12, the channels 15, 16 are opened to the inside of the groove 12a. In the illustrated embodiments, the channels 15, 16 take the form of axial slots opened to the internal face 12 of the annular body 10.

Due to the complexity in the manufacturing of the slots in the axial direction (of the height), the annular body may be produced for example in sintered metallic alloy, thereby achieving the preferred final shape in a more productive and economic way, particularly upon providing the channels 15, 16 in the form of axial slots.

In the embodiment illustrated in figure 1, the channels 15 have a rectangular contour which can be obtained, for example, by machining, in the axial direction, the internal face 12 of the annular body 10 to be formed from a blank of adequate material.

Also, when the ring is obtained for example by powder metallurgy processing and molded to a form close to its final form, the channels 16 may present the approximate form of an opened and rounded "V", with the external ends of its side walls matching with the adjacent convex portions of the internal face 12 of the annular body 10, making the latter present a sinusoidal inner contour or other combination of tangent curves, as illustrated in figure 7.

The constructive alternative illustrated in figures 7

and 8 uses a shape that is better adapted to the manufacturing process by powder metallurgy, resulting in gains of productivity and quality (for the process), since it reduces (the factor of) stress concentration in relation to the rectangular contour illustrated in figure 1 and allows extracting the compacted from the die more efficiently.

Although figures 7 and 8 illustrate the channels 16 with a radial extension insufficient for providing fluid communication between the opposite lateral face portions 11b, spaced from the adjacent walls of the piston P, it should be understood that said channels 16, represented herein in the form of an opened and rounded "V", may be dimensioned for providing said communication according to the form exemplified in figures 1, 2, 3 and 4.

As described above, the channels 15, 16 may be dimensioned with a longer or shorter radial extension, in order to provide communication only between the opposite lateral face portions 11a which are seated against the adjacent walls of the piston groove or also between the opposite lateral face portions 11b of the ring, which are spaced from the adjacent walls of the piston groove. Said channels 15, 16 may present other forms such as trapezoidal, triangular or combinations of tangent curves or others.

It should be understood that the external contact face 13 can be modified by chemical or physical processes or a combination thereof, giving rise to a material layer 13b that is resistant to wear, sticking and friction.

It is a common practice in industries to use transformation of phases, such as in the thermal treatments of quenching and tempering; deposition, whether electrically assisted or not, such as in

chrome-plating or nickel-plating; in the physical vapor deposition and in the chemical vapor deposition; in thermal spraying; temperature-assisted diffusion, as in nitriding, carburizing, boronizing, and ferro-oxidizing, in order to achieve the effect of improving resistance to wear, scuffing and friction.

Specific features of the invention are illustrated in the drawings for convenience only, since each feature may be combined with other features in accordance with the invention. Alternative embodiments shall be construed as possible by those skilled in the art, and are intended to be included in the scope of the claims. Thus, the above description is intended to illustrate rather than limit the protective scope of the invention. All obvious alterations and modifications are within the protective scope as defined by the appended claims.

CLAIMS

1. An oil ring for an internal combustion engine, comprising a metallic annular body (10) to be mounted around a piston (P) reciprocating inside a cylinder (C) of the engine, said annular body (10) having opposite lateral faces (11), an internal face (12) defining a support onto which will be seated a resilient expander (M), and an external contact face (13) to be seated against the internal face of the cylinder (C), characterized in that the external contact face (13) is defined by a single continuous surface extension of the annular body (10) presenting, in the axial direction, a height (h) that is substantially smaller than the height (H) of the internal face (12), each lateral face (11) being defined by at least one lateral face portion (11a, 11b) that is designed to reduce the moment of inertia of the annular body (10) towards its axis and center of mass.
2. The oil ring as set forth in claim 1, characterized in that the height (h) of the external contact face (13) is at maximum about half the height (H) of the internal face (12), in order to allow a corresponding reduction in the tangential load exerted by the ring against the cylinder, without negatively altering the specific pressure exerted by the external contact face (13) against the cylinder.
3. The oil ring as set forth in any one of the claims 1 and 2, characterized in that the external contact face (13) is cylindrical.
4. The oil ring as set forth in any one of the claims 1 and 2, characterized in that the external contact face (13) is defined by a surface with a convex arcuated profile.
5. The oil ring as set forth in any one of the claims

3 and 4, characterized in that the external contact face (13) is symmetrical in relation to a plane that is orthogonal to the axial axis of the annular body (10) and intercepts the latter medianly.

5 6. The oil ring as set forth in any one of the claims 1 and 2, characterized in that the external contact face (13) is conical.

7. The oil ring as set forth in claim 6, characterized in that external contact face (13) has a lowered step
10 (13a) close to its peripheral edge of larger diameter.

8. The oil ring as set forth in claim 1, characterized in that at least one of the lateral faces (11) has at least part of its radial extension defined by a lateral face portion (11a) that is designed to reduce
15 the height of the annular body (10) towards the external contact face (13).

9. The oil ring as set forth in claim 8, characterized in that both lateral faces (11) are at least partially defined by respective lateral face portions (11b)
20 which are mutually convergent towards the external contact face (13).

10. The oil ring as set forth in claim 1, characterized in that at least one of the lateral faces (11) is defined by a first lateral face portion
25 (11a), which is orthogonal to the axial axis of the annular body (10) and maintains the height of the latter equal to the height (H) of the internal face (12), and by a second lateral face portion (11b) extending radially outwardly from the first lateral
30 face portion (11a) towards the adjacent edge of the external contact face (13) of the annular body (10).

11. The oil ring as set forth in any one of the preceding claims, characterized in that the annular body (10) is provided with channels (15, 16) extended
35 by at least portion of the ring height and which are

radially spaced back in relation to the external contact face (13).

12. The oil ring as set forth in claim 11, characterized in that the channels (15, 16) provide
5 fluid communication between lateral face portions (11a, 11b) that are opposite to each other.

13. The oil ring as set forth in claim 11, characterized in that the internal face (12) of the annular body (10) is provided with a circumferential
10 groove (12a) that defines the support for the resilient expander (M), with the channels (15, 16) being opened to the interior of the groove (12a).

14. The oil ring as set forth in claim 13, characterized in that the channels (15, 16) are
15 defined by a plurality of axial slots opened to the internal face (12) of the annular body (10).

15. The oil ring as set forth in claim 14, characterized in that the channels (15) have a rectangular contour.

20 16. The oil ring as set forth in claim 14, characterized in that the channels (16) have a contour with the approximate shape of a rounded and opened "V", with the external ends of its lateral walls matching with adjacent convex portions of the internal
25 face (12) of the annular body (10), giving to the latter a sinusoidal internal contour.

17. The oil ring as set forth in any one of the preceding claims, characterized in that the annular body (10) is made of a sintered metallic alloy.

30 18. The oil ring as set forth in any one of the preceding claims, characterized in that the external contact face (13) is defined by a film (13a) that is made of a material that is resistant to friction, wear and scuffing, provided in the annular body (10).

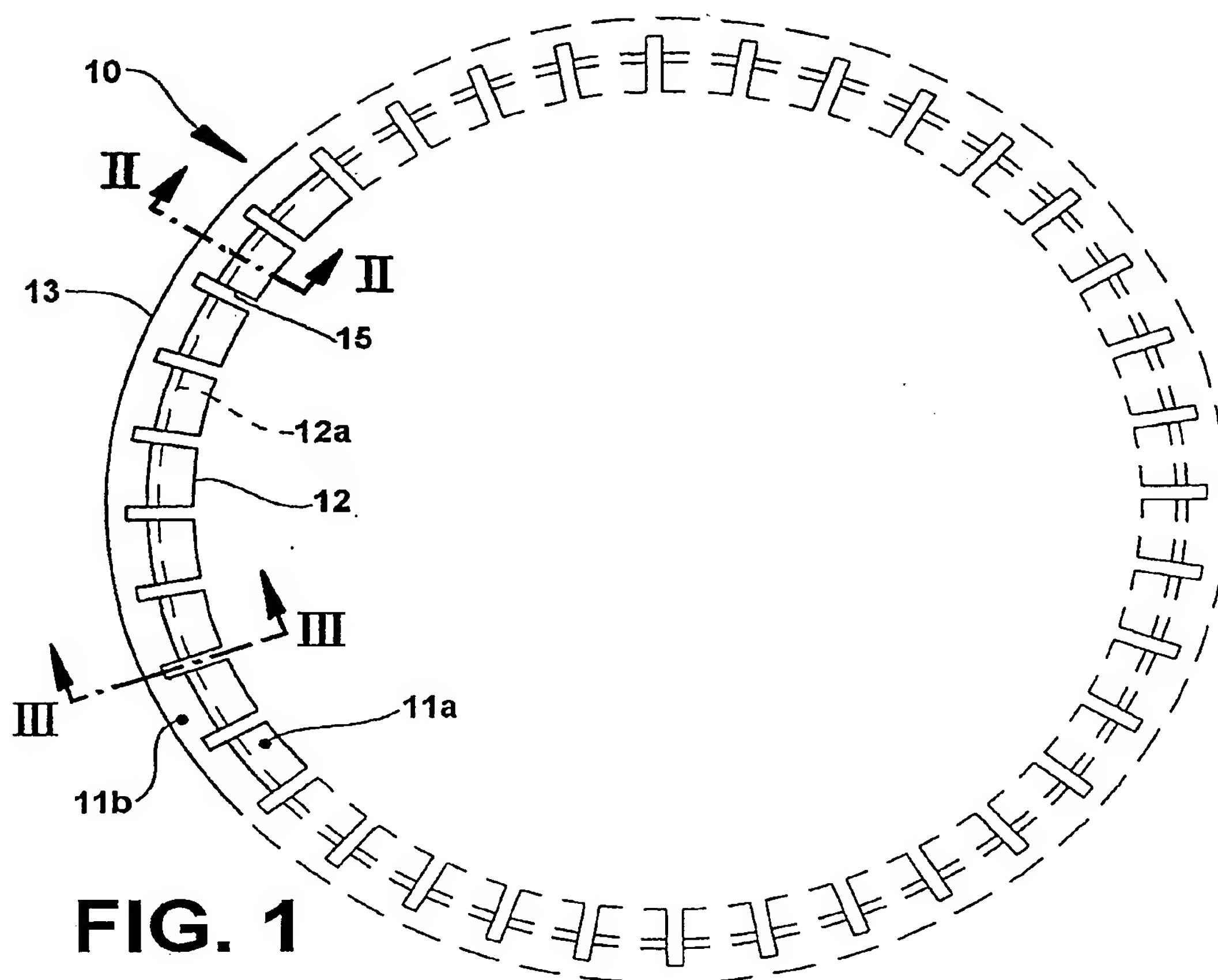


FIG. 1

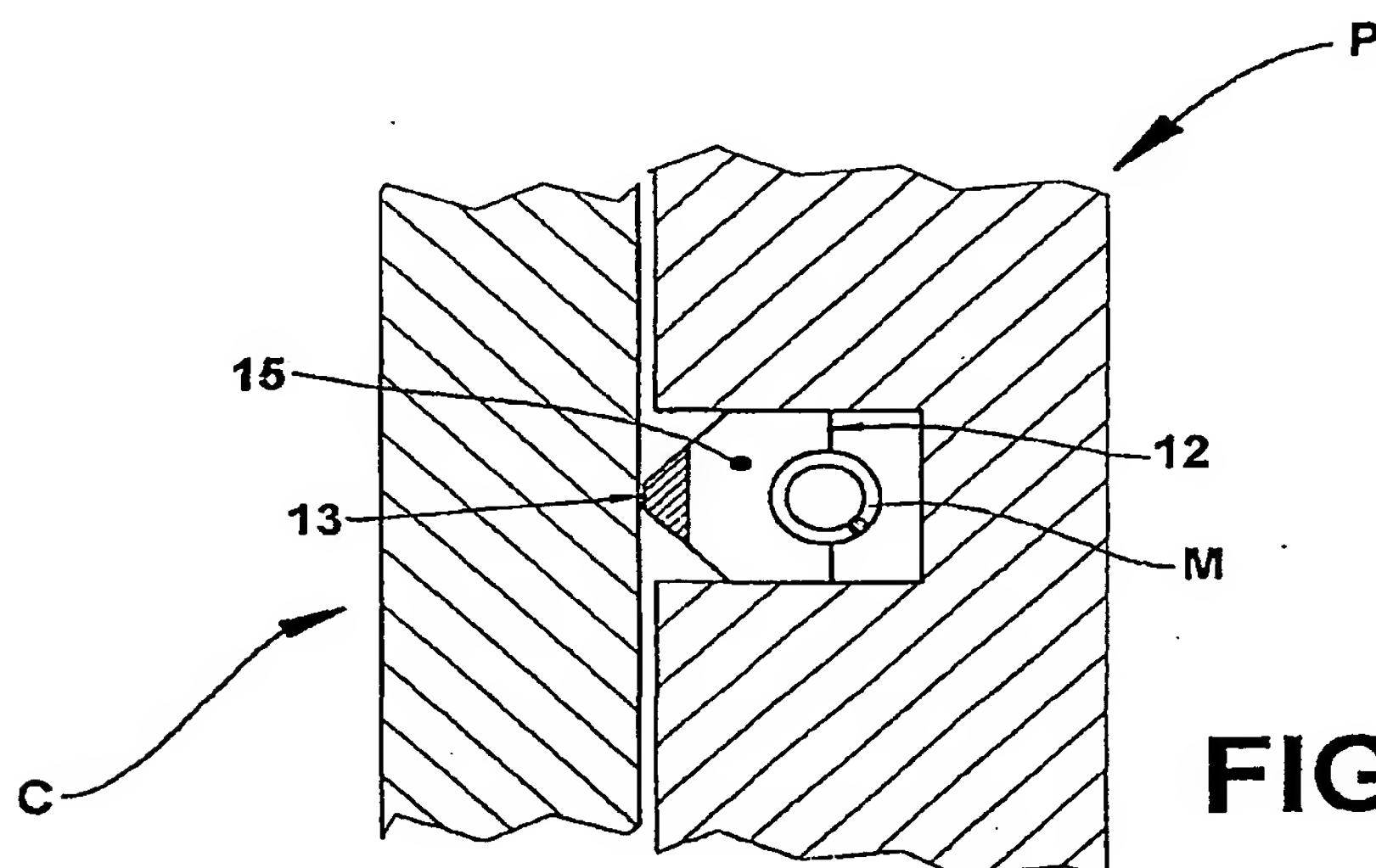


FIG. 3

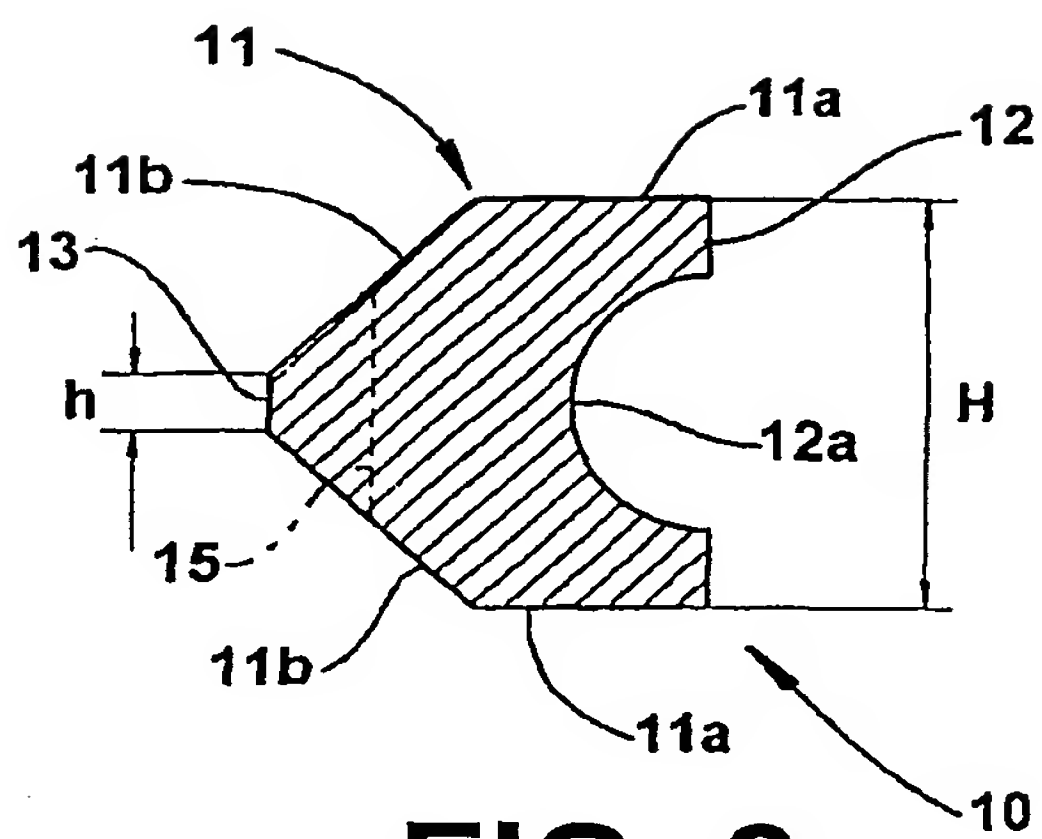


FIG. 2

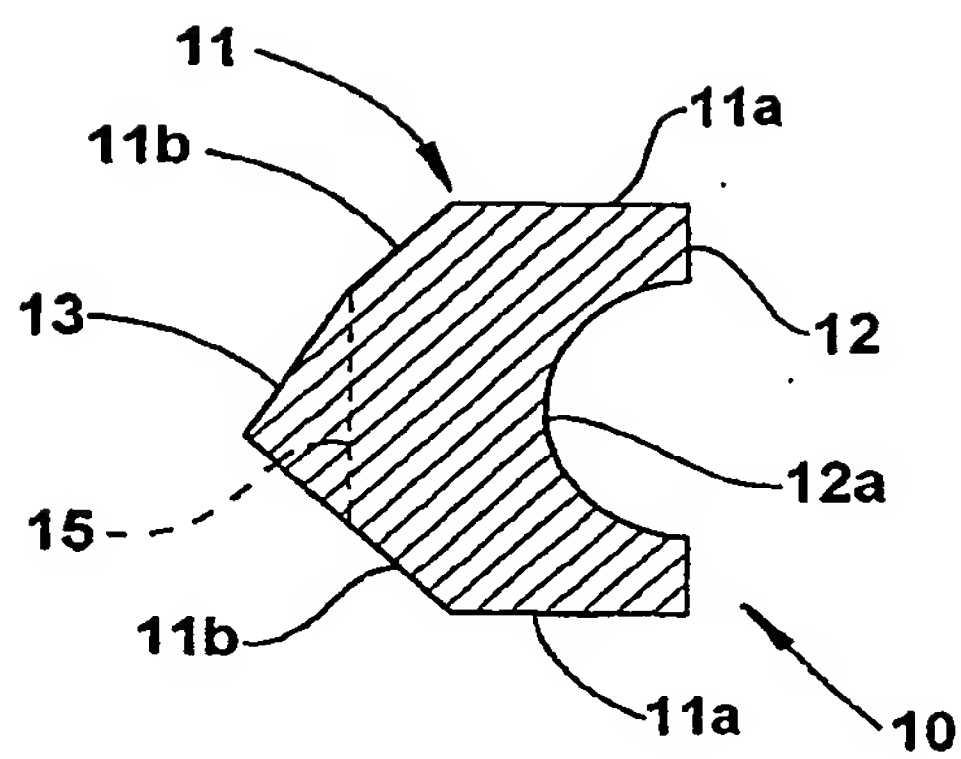


FIG. 4

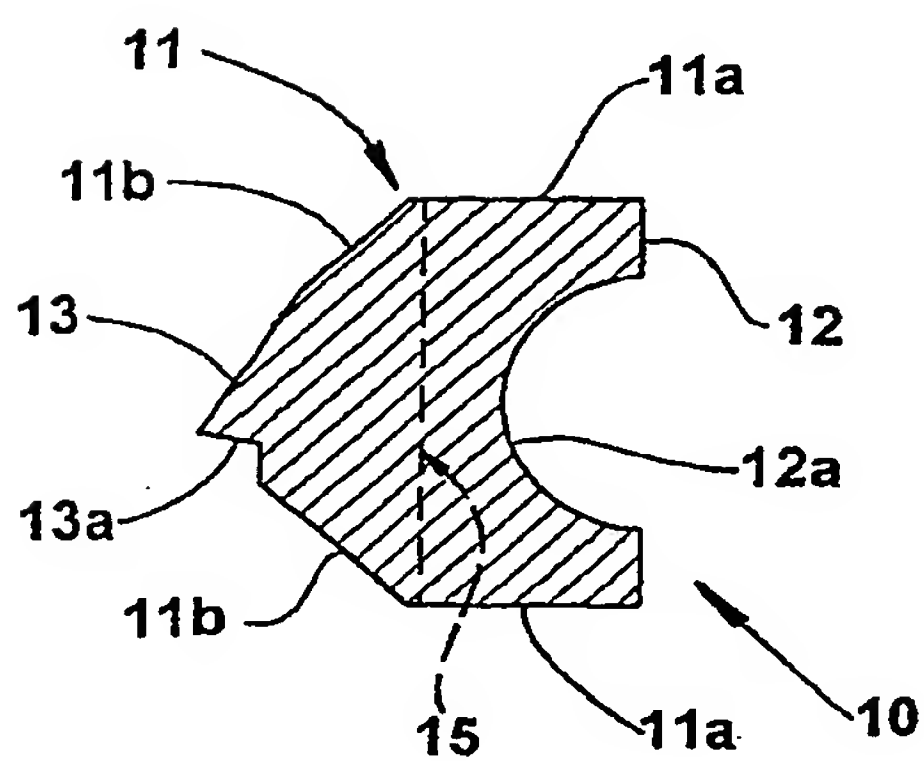


FIG. 5

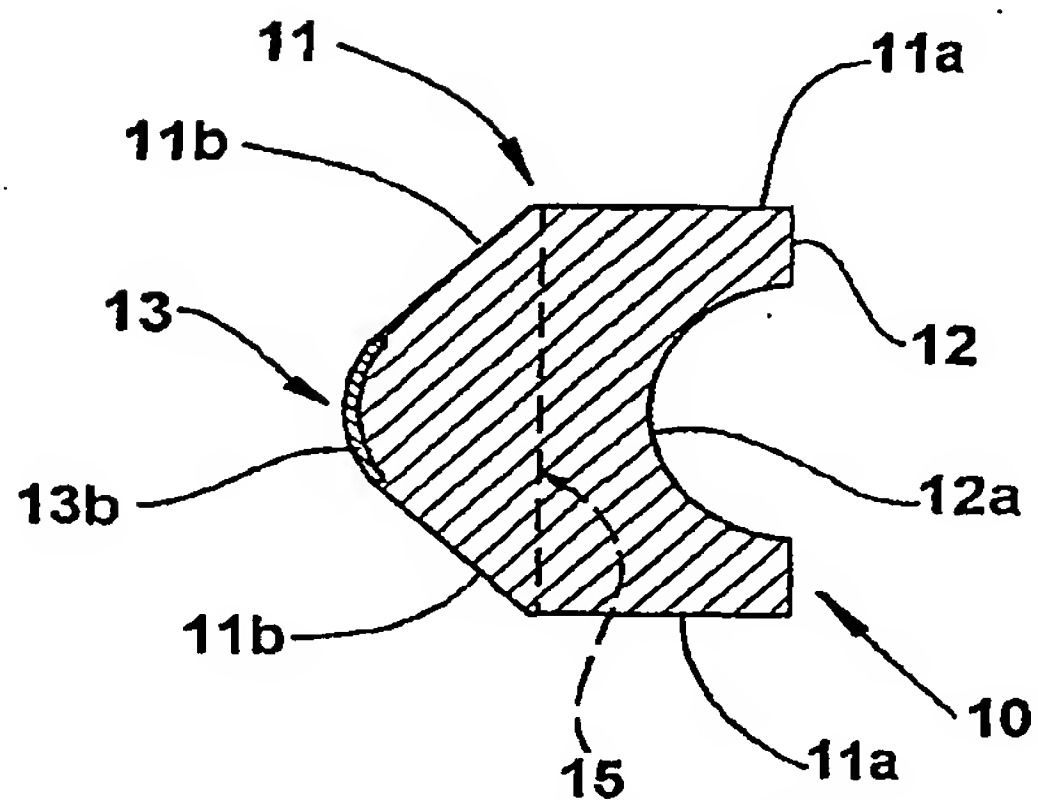


FIG. 6

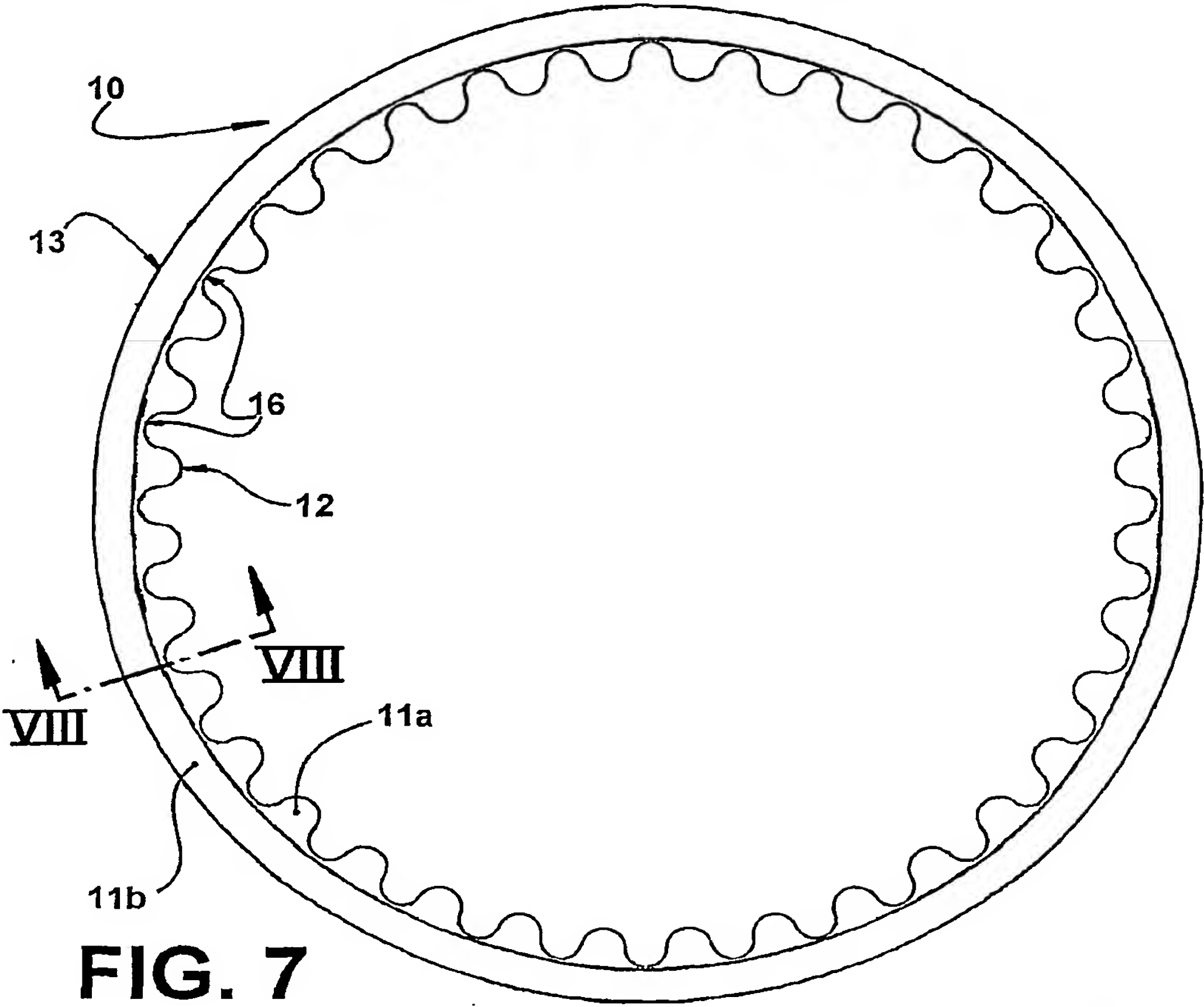


FIG. 7

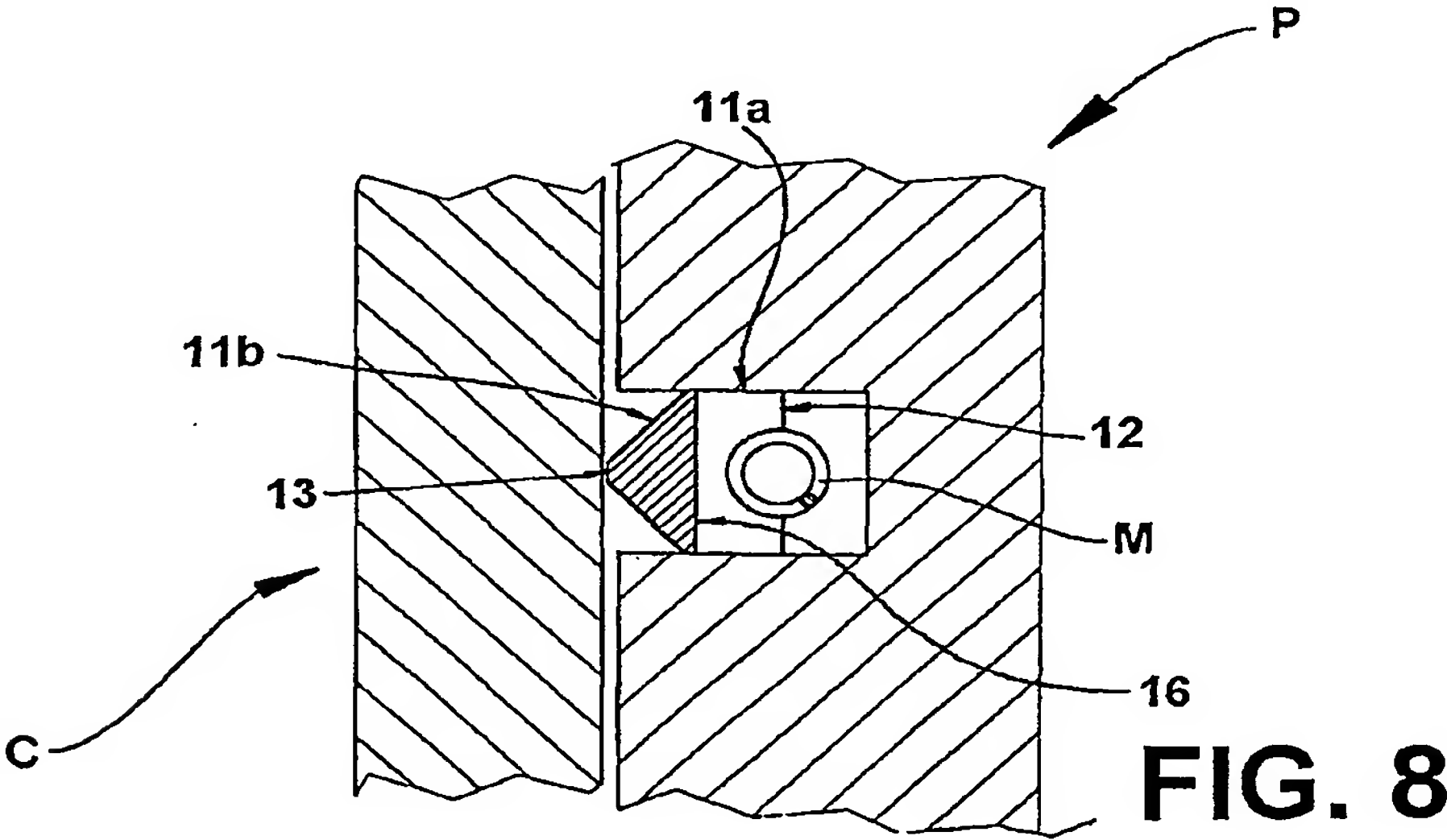


FIG. 8

INTERNATIONAL SEARCH REPORT

Internatic application No
PCT/BR 02/00076

A. CLASSIFICATION OF SUBJECT MATTER

IPC 7 F16J9/20 F16J9/06

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 7 F16J

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

WPI Data, PAJ, EPO-Internal

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	DE 85 03 197 U (GOETZE AG) 21 November 1985 (1985-11-21) page 4, line 15 -page 5, line 22; figures 1,2	1-3,5, 8-10,17, 18
Y	---	4
X	DE 197 55 425 A (FEDERAL MOGUL BURSCHEID GMBH) 17 June 1999 (1999-06-17) abstract; figure	1-3, 8-10,17, 18
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INTERNATIONAL SEARCH REPORT

Internat. Application No
PCT/BR 02/00076

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	EP 0 544 459 A (DANA CORP) 2 June 1993 (1993-06-02) abstract; figures 1A,1B and detail 54	1-3, 8-11,13, 17,18
Y	---	6,7
Y	DE 38 33 322 A (COFAP) 7 December 1989 (1989-12-07) abstract; figure 1	4
Y	---	
Y	DE 36 06 011 A (MUELLER HEINZ KONRAD PROF DR I) 17 September 1987 (1987-09-17) figure 3	6,7
A	---	
A	US 2 291 945 A (BOWERS THOMAS A) 4 August 1942 (1942-08-04) figures 5-8 -----	11-16

INTERNATIONAL SEARCH REPORT

Information on patent family members

International

Application No

PCT/BR 02/00076

Patent document cited in search report		Publication date	Patent family member(s)	Publication date
DE 8503197	U	21-11-1985	DE 8503197 U1	21-11-1985
DE 19755425	A	17-06-1999	DE 19755425 A1	17-06-1999
EP 0544459	A	02-06-1993	BR 9204209 A	01-06-1993
			EP 0544459 A1	02-06-1993
			JP 5240348 A	17-09-1993
			MX 9206749 A1	01-05-1993
			US 5618046 A	08-04-1997
DE 3833322	A	07-12-1989	BR 8802641 A	09-01-1990
			DE 3833322 A1	07-12-1989
DE 3606011	A	17-09-1987	DE 3606011 A1	17-09-1987
US 2291945	A	04-08-1942	NONE	